# Preliminary Engineering Report

Scenic Rim Agricultural Industrial Precinct

5103/57-001

Prepared for Kalfresh Pty Ltd

25 September 2023





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# **Executive Summary**

Kalfresh Pty Ltd has commisioned Stantec (Qld) Pty Ltd (Stantec) to provide preliminary civil engineering advice to support the proposed Scenic Rim Agricultural Industrial Precinct (SRAIP) Development Approval application to create an agricultural industrial precinct at 6200-6206 Cunningham Highway, Kalbar, Scenic Rim. The proposed development is referenced as 'The Scenic Rim Agricultural Industrial Precinct (SRAIP)' and intends to create a formal hub for fresh and frozen food production in an agricultural region 84km southwest of Brisbane.

This report includes recommendations for the civil works required to create a developable land formation for the proposed industrial allotments and road corridors. The civil works proposed to facilitate the development includes bulk earthworks, roadworks, stormwater drainage, stormwater quantity management, stormwater quality management, water reticulation and sewerage infrastructure.

This report also includes preliminary stormwater calculations in relation to the composting facilities to the west of the main industrial development.

The preliminary engineering recommendations and design considerations documented by Stantec are summarised in this report.

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## 1 Introduction

Kalfresh Pty Ltd has commissioned the services of Stantec (Qld) Pty Ltd to prepare preliminary engineering advice to support the Development Approval application for the proposed Scenic Rim Agricultural Industrial Precinct (SRAIP) at 6200-6206 Cunningham Highway, Kalbar, 4 km west of Kalbar, and 84km south-west of Brisbane. This engineering review has been completed based upon the relevant Scenic Rim Regional Council Planning Scheme Policies and the RPS Plan Ref No. 142489-06T included within **Appendix A**.

Kalfresh Pty Ltd proposes to create a fully integrated agricultural processing precinct (the SRAIP) at the existing Kalbar operating base. The SRAIP proposal provides approximately 40 hectares of developable land for rural industrial infrastructure primarily for the packing and production of high value secondary produce and the ancillary services and infrastructure required to operate such a precinct. The existing Kalfresh operations will remain on the site and be expanded to meet market demand.

It is proposed to reconfigure six existing allotments located at 6200-6206 Cunningham Highway, including:

- > Lot 2 on SP192221;
- > Lot 3 on SP192221;
- > Lot 4 on SP192221;
- > Lot 2 on RP 20974;
- > Lot 1 on RP216694; and
- > Lot 2 on RP44024.

The six existing allotments subject to this Development Approval application encompass a total site area of approximately 250 ha. The subject allotments are bounded by the Cunningham Highway to the east, agricultural lands to the north and south, and a quarry to the west. Figure 1-1 indicates the locality of the subject allotments.

Figure 1-1 Site Location



The proposed development area topography is relatively flat with a gradual fall towards the northern boundary at a grade of circa 1:300 (0.33%). The maximum ground elevation is 84.0m AHD at the southern boundary whilst the minimum ground elevation is 81.0m AHD at the northern boundary. There is an existing overland flow path running along the western extents of the proposed development area which will be reconfigured to cater for the 1% AEP flood event as part of the proposed works. The land towards the rear of the property, outside of the development footprint and on the opposite side of the overland flow path, rises sharply towards the western boundary.

Figure 1-2 below provides an overview of the proposed development area.

Figure 1-2 Development Site Area



# 2 Civil Works

#### 2.1 Clearing & Site Preparation

The site development area currently consists of agricultural cropping land and the existing Kalfresh production facilities. The development of this site necessitates that the area is cleared completely of any existing vegetation including the removal of any unsuitable material identified prior to the commencement of bulk earthworks and civil works construction.

It is recommended that the early establishment of erosion and sediment control measures is carried out in conjunction with the commencement of clearing works in order to prevent the discharge of soils from the site and protect existing downstream infrastructure.

#### 2.2 Earthworks

Bulk earthworks will be completed across the subject site to create a developable land formation in accordance with Stantec sketch 510357-001-CI-1010. This earthwork operation will include the stripping/ stockpiling of topsoil and reshaping of land to generally achieve the proposed site levels across the development. In addition, Stantec have prepared a bulk earthworks engineering set of drawings which are also included in this application.

Based upon Stantec's experience within the Scenic Rim region and surrounding areas, coupled with the elevated site levels, it has been assumed that the site is devoid of acid sulphate soils and contaminated land.

The preliminary earthworks design comprises of filling the site above the 1% AEP flood level (plus climate change allowance) with an additional 300mm freeboard provided. This will require additional material which is proposed to be obtained from the deepening of the flood diversion channel and from within on-site borrow pits. Hence, the haulage distance of fill material will be limited to within the existing allotment boundaries and haulage of material from outside the subject site will be minimal.

The earthworks design based upon the proposed development layout indicates that the earthworks operation will comprise approximately 489,000m<sup>3</sup> cut to fill onsite and 217,000m<sup>3</sup> of additional fill required which will be obtained from borrow pits within the subject site (locations indicated on drawing 510357-001-CI-1010).

The proposed earthworks profile has been created with the intent to minimize the amount of fill whilst ensuring the development can be appropriately serviced by a stormwater drainage network and also be resilient to the 1% AEP flood event.

All earthworks on the site will be carried out in accordance with Level 1 supervision and testing requirements, with any existing dams and/or unsound materials being removed and replaced under Level 1 supervision.

It is also recommended that prior to the de-commissioning of all sediment basins, all collected silt and unsuitable material should be removed from the site and the basin area rehabilitated using a high quality of fill material in order to ensure long-term stability to this area of the site.

The Stantec sketch 510357-001-CI-1010 included in **Appendix B** of this replot illustrates the proposed cut and fill zones.

#### 2.3 Erosion & Sediment Control

In accordance with IECA Best Practise Guidelines and Scenic Rim Council standards, it is proposed that in conjunction with the Operational Works Application phase of development a detailed Soil Erosion and Sediment Control Plan will be prepared in order to address the specific measures to be implemented manage erosion onsite and limit sediment discharge offsite. During the construction phase, the Contractor is to have a certified erosion and sediment control plan on site at all times.

General measures to be implemented during the construction phase in order to prevent the erosion of sediment from the site are as follows:

- Contractor to achieve temporary, interim or permanent ground cover to disturbed earthworks areas as soon as practicable;
- Sediment filter fencing is to be located at the downstream end of all open earthworks to remove sediment from overland flow prior to discharging off site;
- Truck shake down areas shall be provided to remove any loose materials from vehicles prior to departure from the site;

- All sediment control structures must be maintained in an effective operational condition.
   These structures must not be allowed to accumulate sediment volumes in excess of forty percent of the sediment storage design capacity;
- If topsoil will be stripped and stockpiled, perimeter silt fences are to be installed around the stockpile areas to prevent the material discharging from the site;
- All sediment control structures are to be supplied and installed in accordance with Scenic Rim Regional Council planning scheme policies and IECA Best Practice Guidelines; and
- A sediment pond is to be constructed to suit the construction site profile and sized appropriately to capture the require volume of sediment laden runoff.

#### 2.4 Roadworks

An internal road network will be created in order to provide access to each of the proposed industrial allotments and access and egress from the overall development. There are two proposed road profiles within the development, including:

- Road 1: consists of a 30.3m wide road reserve with an 14m carriageway which consists of 3.5m traffic lane and 3.5m parking bays.
- Road 2: consists of a 40m wide road reserve with 2 x 8m wide carriageways on either side of a 15m wide grass swale. The introduction of the grass swale between the 7m carriageways will used to capture major stormwater flows from the adjoining road and lots. The 8.0m carriageways consist of a 3.5m traffic lane, a 3.5m parking bay and a 1m shoulder adjacent the swale batter. 4.5m wide verges with 1.5m wide pathways are provided on each side.

These sections reflect a modified version of an 'Industrial Collector Street' profile as shown in Figure 9.7.A of IMEAQ Queensland Streets.

The main collector street traverses the centre of the site with a cul-de-sac provided at the south-west of the alignment to facilitate turning movements. This layout provides access to each lot whilst ensuring sufficient manoeuvrability for Class 10 (B-double) trucks within the industrial estate.

Provision for a future road connection towards the north-west of the site has also been facilitated within the layout. The proposed road will traverse the waterway channel via a weir structure. The design intention of the weir is to (a) allow safe crossing of the overland flow channel by vehicles accessing the north-west of the subject site, and (b) act as a flood mitigation device which restricts regional flows within the channel below the 10% AEP level. The weir will be constructed with 2 x 2400(W) x 300(H) RCBC culverts. These will be set at the IL of the waterway diversion channel to allow low flows within the channel to free-drain. A section of the weir is provided on Stantec sketch 510357-001-CI-1300.

Access to the development will be provided by a new intersection onto the Cunningham Highway located circa 460 m to the north-east of the existing access point. The intersection layout and geometry will be designed to TMR standards and will accommodate Class 10 (B-double) vehicles. A right-turning lane will be provided on the Cunningham Highway for vehicles entering the site. Within the site, no direct lot access will be permitted within 50 metres of the new Cunningham Highway intersection.

The 3 No. existing access points on to the Cunningham Highway currently utilised by Kalfresh will be decommissioned. The proposed access arrangement will provide significant road safety benefits to the surrounding road network.

#### 2.5 Stormwater Quantity Management

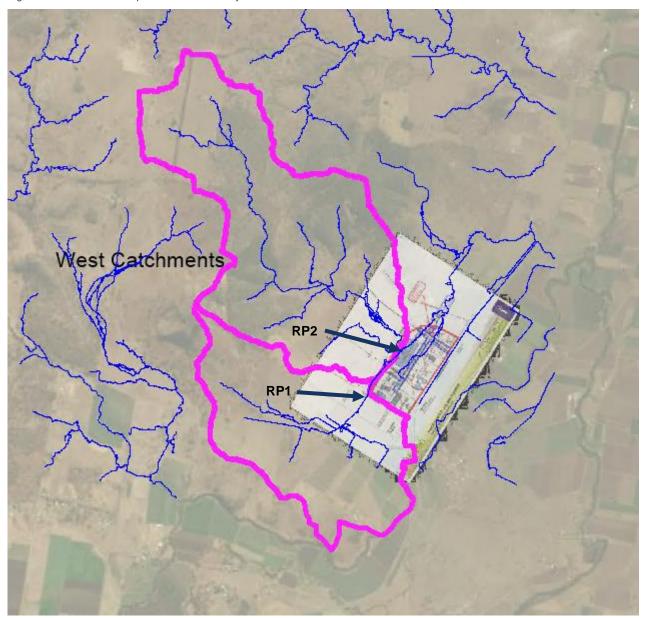
The stormwater quantity management strategies and outcomes for the proposed development are outlined by the Scenic Rim Agricultural Industrial Precinct Integrated Water Management Plan prepared by Stantec, and included in the submission under separate cover.

The objective of the stormwater management plan is to ensure that the effect of delivering the proposed development achieves a no worsening of post-development runoff compared to the runoff experience predevelopment.

It has been identified that the subject site is located at the confluence of 2 No. existing stormwater catchments denoted RP1 & RP2 illustrated in Figure 2-1 below. Under existing conditions RP1 and RP2 are diverted around the existing Kalfresh facilities before discharging to Warrill Creek to the north east of the site via a series of local watercourses.

In order to achieve no worsening of stormwater discharge it is proposed that stormwater detention basins will be provided at the low point of each developed catchment to restrict runoff prior to outfall. The Integrated Water Management Plan outlines that the proposed strategy to achieve no-worsening of pre-development runoff is to detain the runoff generated from the developed site in the proposed flood conveyance channel running along the western boundary of the development pad. This conveyance channel will act as a detention basin and has largely been split into two sub-basins. These basin areas have been sized such that overall post-development peak flows discharging from the site are limited to or are less than the pre-development flows. Please refer to Section 4.1.3 of the Integrated Water Management Plan report for additional details on the proposed stormwater quantity (detention) management strategy.

Figure 2-1 Pre-Development Catchment Layout



All stormwater runoff within the site catchment shall be captured and directed into the stormwater detention basins via a mix of conventional piped network and open channel (grass swale) drainage infrastructure where the basins shall be constructed in accordance with the findings of the Integrated Water Management Plan.

The open channel or 'central road swale' has been sized to cater for peak flows from the 1 in 100 year ARI (with climate change factor allowed). The maximum water depth in the swale is 1.109m in the 1 in 10 year ARI and 1.479m in the 1 in 100 year ARI event.

The findings of the stormwater management plan recommend that the detention basins are constructed in accordance with the parameters outlined below:

Table 2-1 Proposed Detention Basin Properties

Parameter	Upstream Basin	Downstream Basin
Basin base area	285 m2 at 80.3m AHD	490 m <sup>2</sup> at 80m AHD
Basin top area	69,440 m <sup>2</sup> at 81.3m AHD	63,192 m <sup>2</sup> at 80.8m AHD
Basin height	1.3m	0.8m
Total Volume at top of basin	18,324 m <sup>3</sup>	17,250 m <sup>3</sup>
Low flow outlet	2 x 2.4m x 0.3m box culverts	2 x 0.9m x 0.3m box culverts
High flow outlet	Access road at 81.3m AHD, acting as a weir	Northern bund at 80.8m AHD, acting as a weir

The low flow outlets (RCBC's) and high-level spillway (weir) shall be provided as per the details above. The low flow outlet will be set at the base of each detention basin allowing each basin to empty completely following a storm event. To ensure compliance with the Water Plan (Moreton) 2007 all basins will discharge down completely with no retention storage provided.

The conceptual stormwater drainage layout which includes the developed catchment areas has been provided for information only and is illustrated in Stantec sketch 510357-001-CI-1300 included in **Appendix B** of this report. The conceptual stormwater drainage layout also includes and shows the water quality outlets coordinates and legal point of discharge.

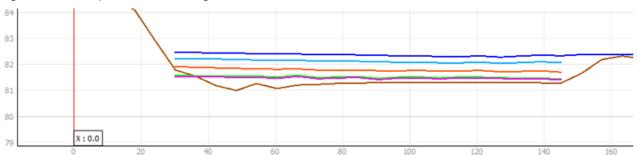
#### 2.5.2 Weir Crossing Flood Characteristics

The flood events have also been modelled to simulate the flood heigh and velocity over the proposed stormwater weir crossing (Upstream Basin outlet) which provides road access to the north-west areas of the site. The summary of these results can be seen in Table 2-3 below. Additionally, the flood height can be seen below in figure 2-2 on a sample profile below for each of the respective storm events.

Table 2-2 Flood Event Heights and DV over Weir

Event	Flood Height (mAHD) Mean	DV (mean) m²/s
100yCC	82.332	2.76
100Y	82.081	2.03
50Y	81.731	1.094
<b>20</b> Y	81.439	0.236
10Y	81.400	0.148

Figure 2-2 Sample Profile of Flow Heights over Weir



As shown, the weir overtops by 148mm during the 1 in 10 year ARI with a DV (depth velocity product) of 0.148. As per QUDM Table 7.4.3, a DV <0.3 m²/s is considered safe to traverse. The depth of overtopping (and associated DV) in events exceeding a 1 in 20 ARI are **not** considered trafficable.

# 2.6 Stormwater Quality Management

The stormwater quality management strategies and outcomes for the proposed development are outlined by the Scenic Rim Agricultural Industrial Precinct Integrated Water Management Plan, included under Appendix L of the submission.

A stormwater management strategy has been prepared outlining the water treatment measures required to be implemented in order to treat stormwater runoff from the development and achieve the stormwater quality objectives required by State and Council Planning Policies.

The proposed stormwater management strategy comprises the construction of bio-retention systems to treat stormwater runoff so that the overall pollutant load reduction meets the individual pollutant load reduction target. Each allotment will be treated on an individual basis via a bio-retention system installed prior to the discharge point of each lot. The use of proprietary stormwater quality systems may also be utilised in lieu of a bio-basin subject to planning approval.

MUSIC modelling has been completed for the internal road network in order to verify that the proposed treatment trains and bio-retention basin parameters will achieve the required water quality objectives. Table 2-2 below outlined the proposed bio-retention basin properties.

Table 2-3 Proposed Bio-Retention Basin Properties

Parameter	Bio-retention Basin
Extended Detention Depth (m)	0.2
Saturated Hydraulic Conductivity (mm/hr)	200
Filter Depth (m)	0.4
Filter Area (m²)	varies, refer Table 12 of Stantec IWMP Plan
TN Content of Filter Media (mg/kg)	400
Orthophosphate Content of Filter Media (mg/kg)	30
Total Filter Area Required	6,798 m <sup>2</sup>

Further details of the MUSIC model are provided in the Integrated Water Management Plan report.

#### 2.7 Sewerage Reticulation

The proposed development will operate self-sufficiently in relation to sewerage reticulation, treatment and disposal. Therefore, no agreement or planning approval will be sought from Queensland Urban Utilities.

An internal sewerage network is to be constructed from NuSewer (PE) in accordance with the provisions of the SEQ Code. Where possible all allotments within the development have been graded such that they may be serviced by sewer located within the road reserve at the front of the allotments. A pressurized vacuum sewerage system may be installed should the depth of a gravity sewerage system become un-viable.

It is proposed the wastewater flows generated within the proposed development will be discharged to the onsite wastewater treatment plant (WWTP). Details of the on-site wastewater treatment plant are provided in Precise Environmental's 'Onsite Wastewater Management Report' which is included in this application under separate cover. The storage capacity of the WWTP is 200 kL, which has been sized using the Peak Wet Weather Flow (PWWF =  $5 \times 40 \text{ kL} = 200 \text{ kL}$ ).

The WWTP has been designed to treat sewerage to a Class B standard as per Queensland Water Recycling Guidelines (EPA 2005) and the Public Health Regulation 2005 (QLD). Treated sewerage will then be piped to the proposed irrigation area to the north-west of the industrial precinct.

The development will have a maximum of 800 staff working for the industry supplying and distributing vegetables. Sewerage generation estimates were based on the 'AS/NZS 1547:2000 Appendix 4.2D Typical Domestic Wastewater Flow Design Allowances (Rural Factories). This reference states that the maximum sewage generation rate is 50 L/d per staff member. Based on maximum rate, the average dry weather flow (ADWF) is  $50 \times 800 = 40,000 \text{ L/d} = 0.46 \text{ L/s}$ .

The conceptual sewer reticulation layout has been provided for information only and is illustrated in Stantec sketch 510357-001-CI-SK103 included in **Appendix D**. The conceptual sewer reticulation also includes the indicative wastewater treatment plant location in addition to the proposed irrigation area.

#### 2.8 Water Reticulation

It is proposed that the development will be serviced by two watermains, consisting of:

- A conventional potable pressure water reticulation system treated to drinking standard; and
- A recycled watermain network for industrial and/or processing uses.

It is proposed that the internal water reticulation will be supplied by existing bores on the site. Kalfresh are currently in discussions with Department of Natural Resources, Mines and Energy in relation to securing alternative high priority water sources. Stantec understands that a high priority water license has been obtained by Kalfresh from SEQ Water for an allocation from the Warrill Creek. It is proposed that water from the Warril Creek will be pumped to a water storage dam on site before being treated and reticulated internally

Ultimately, it is intended that the proposed development will operate self-sufficiently in relation to potable water. Therefore, no agreement or planning approval will be sought from Queensland Urban Utilities.

The conceptual water reticulation layout has been provided for information only and is illustrated in Stantec sketch 510309-002-CI-SK100-102 included in **Appendix D**. The conceptual water reticulation also includes the indicative location of the water treatment plant in addition to the alignment from the site to the water intake point at the Warrill Creek. The sketches also show the proposed alignment of the raw water from the internal bored and the Warrile Creek, treated water and recycled water mains.

## 2.9 Composting Pad

Stantec have undertaken preliminary stormwater calculations in order to size the leachate ponds and stormwater basins required to capture runoff from the compost pads.

An overview of the concept stage stormwater functional layout plan for the compost pad area is provided in **Appendix C of this report**. The composting pad area will be bunded to divert overland flows from outside the pad around the perimeter.

# 3 Conclusion

From the investigations carried out it is considered that this site can be serviced by the proposed internal infrastructure and that the site may be suitably engineered in accordance with the relevant Scenic Rim Regional Council and Queensland State Government Planning Scheme policies, standards and guidelines to achieve the proposed development detailed by the RPS Plan of Subdivision.

Stantec therefore consider that the site is suitable for development in accordance with the proposed Development Approval application.

APPENDIX



PLAN OF SRAIP





APPENDIX

В

PRELIM ENGINEERING SKETCHES





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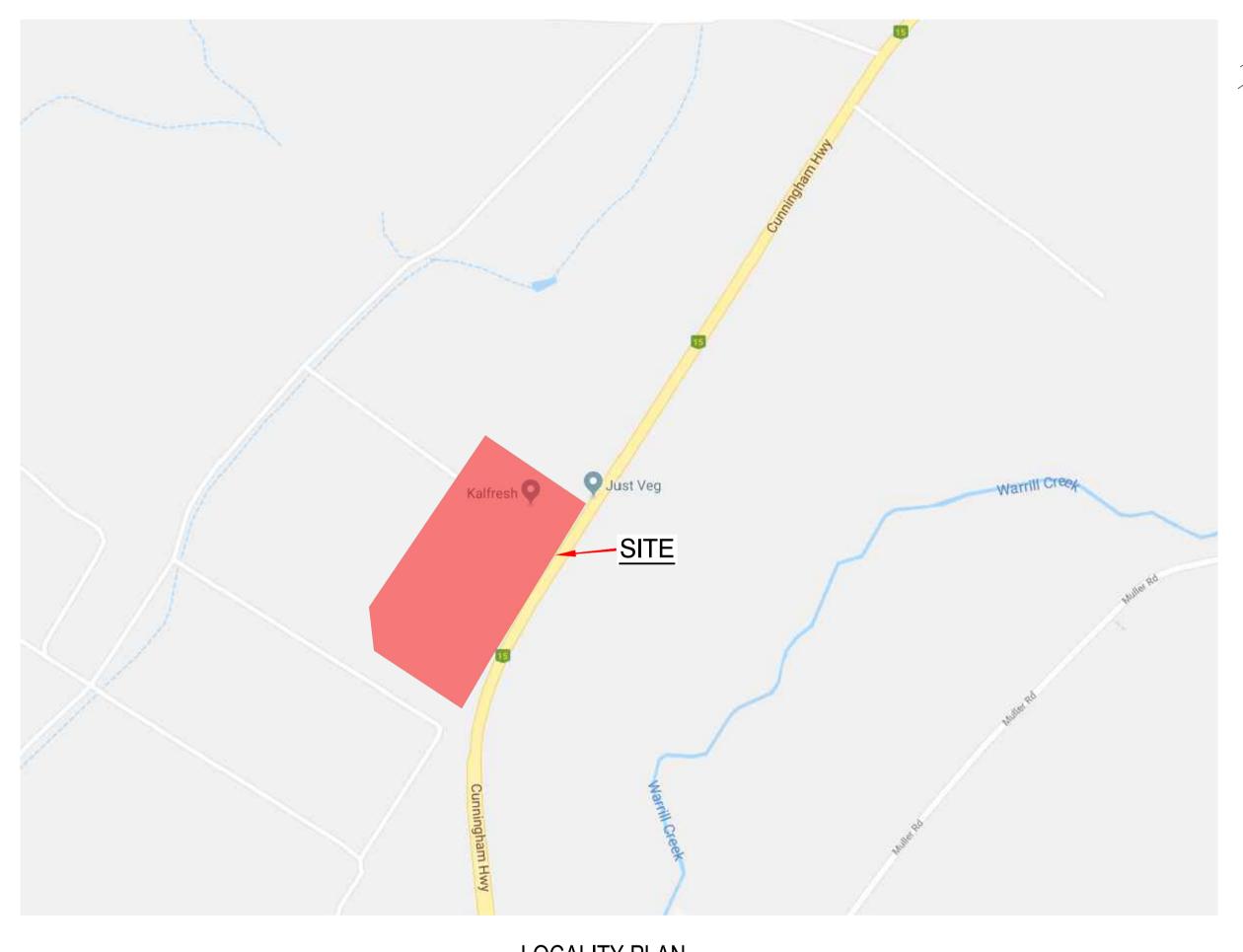
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SCHEDULE OF DRAWINGS		
DRAWING No.	DESCRIPTION	
510357-001-CI-1000	COVER SHEET	
GENERAL		
510357-001-CI-1001	DRAWING SCHEDULE AND LOCALITY PLAN	
510357-001-CI-1010	BULK EARTHWORKS LAYOUT PLAN	
510357-001-CI-1011	ROAD TYPICAL CROSS SECTIONS	
510357-001-CI-1015	BULK EARTHWORKS SECTIONS SHEET 1	
510357-001-CI-1016	BULK EARTHWORKS SECTIONS SHEET 2	
ROADWORKS		
510357-001-CI-1100	MC01 LONGITUDINAL SECTION	
510357-001-CI-1101	MC02 LONGITUDINAL SECTION - SHEET 01	
510357-001-CI-1102	MC02 LONGITUDINAL SECTION - SHEET 02	
STORMWATER DRAIN	IAGE	
510357-001-CI-1300	STORMWATER LAYOUT PLAN	
SEWER RETICULATION		
510357-001-CI-1500	SEWER RETICULATION LAYOUT PLAN	
WATER RETICULATION		
510357-001-CI-1600	WATER RETICULATION LAYOUT PLAN	





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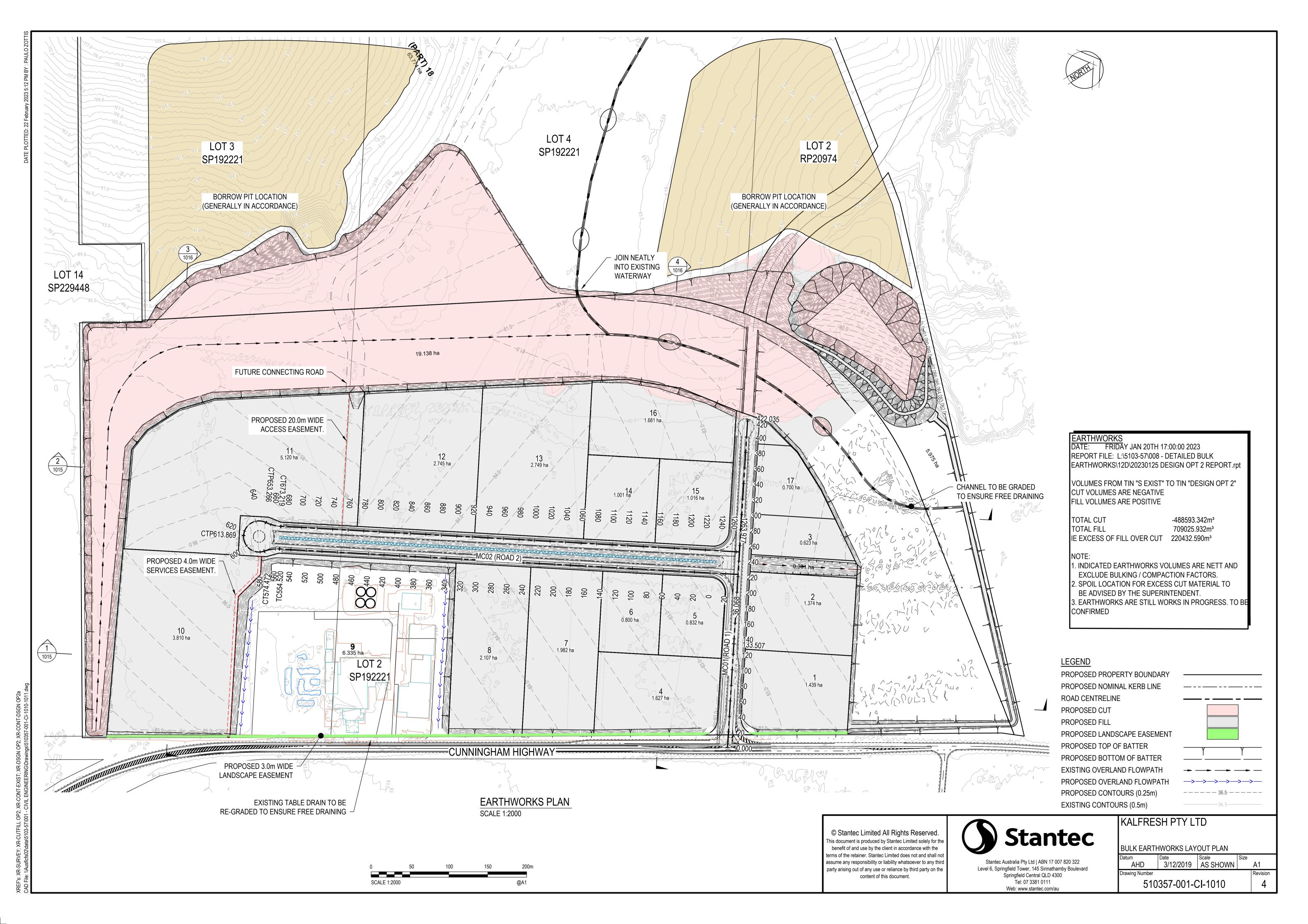
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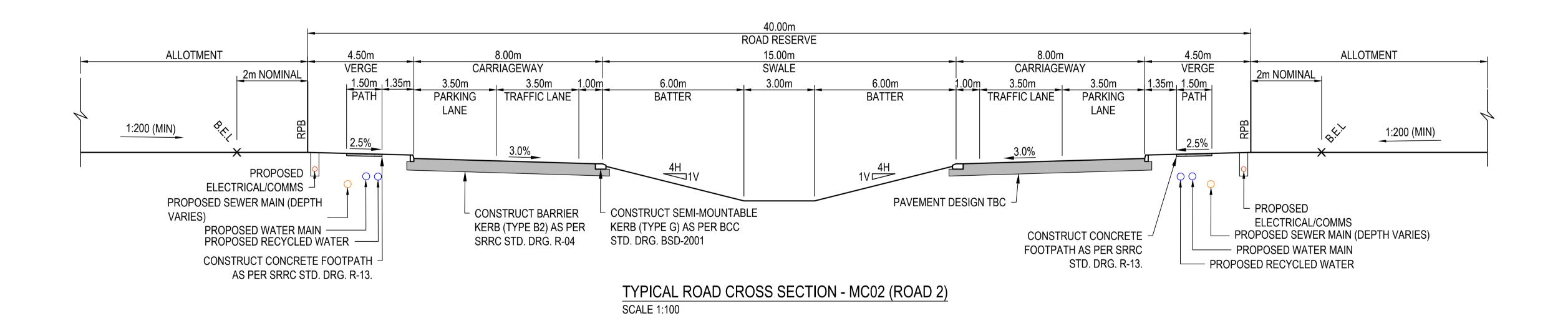
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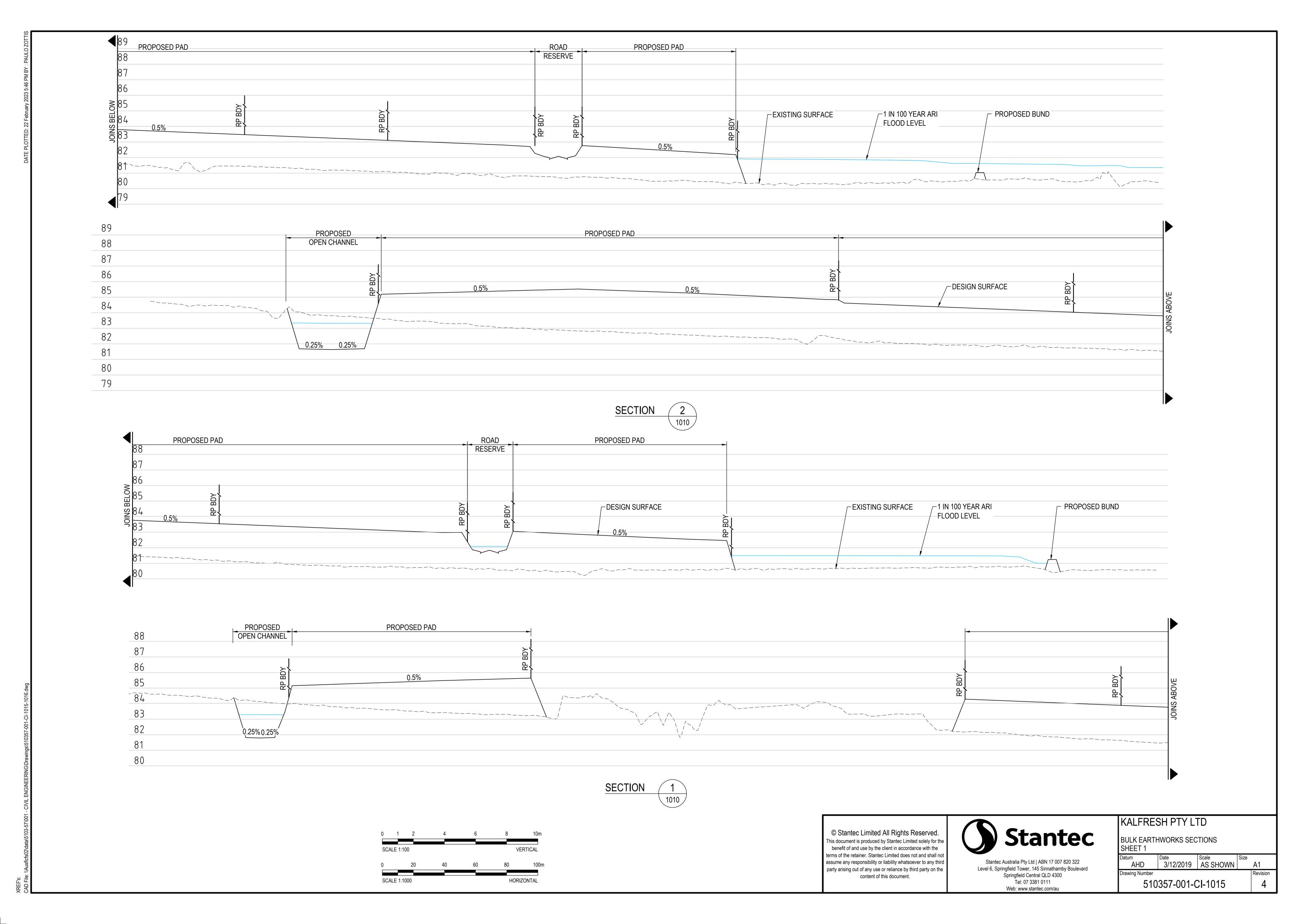


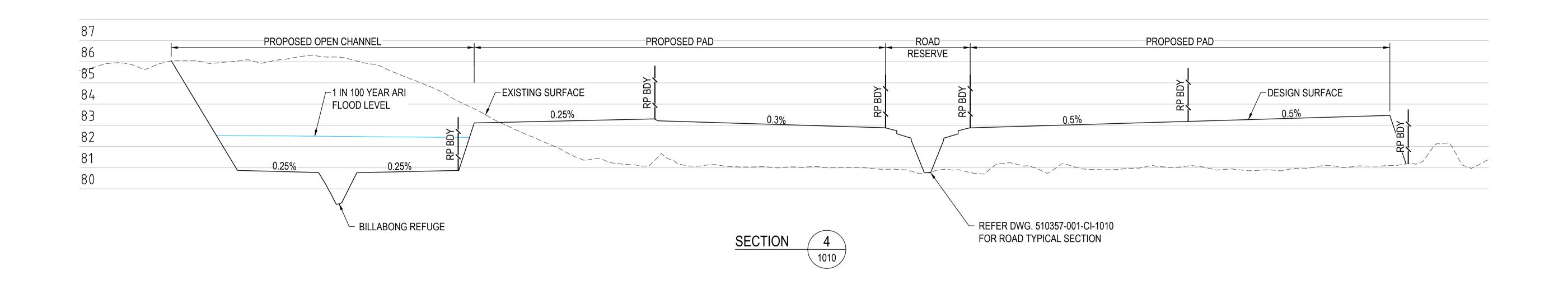
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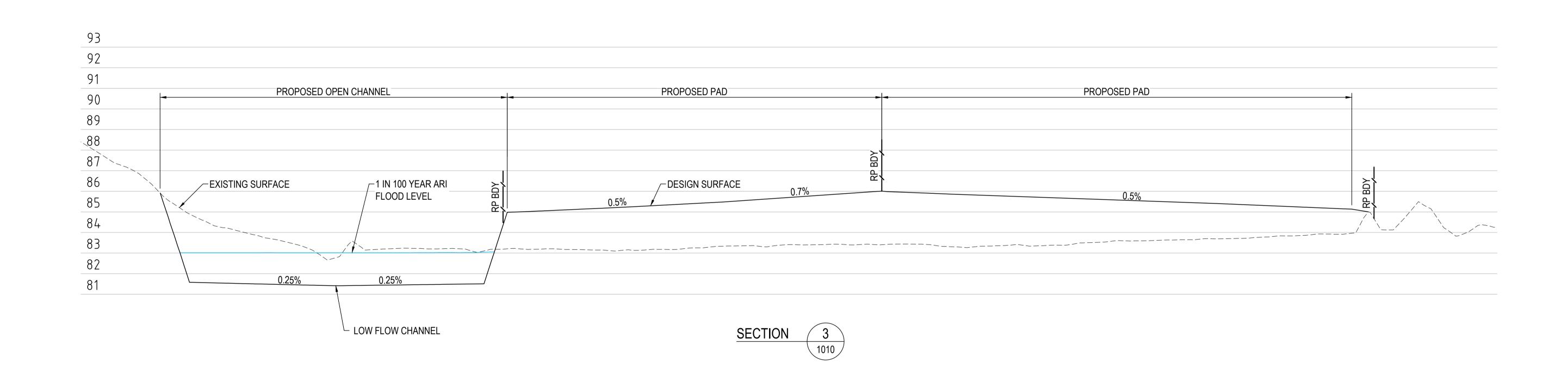
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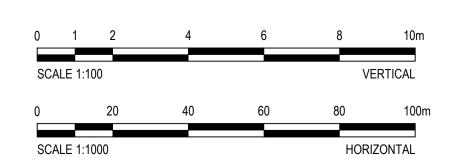
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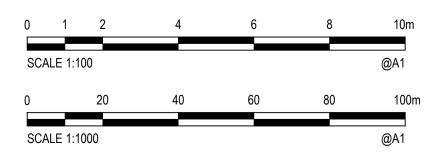
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EXISTING SURFACE DESIGN SURFACE VTP CH -29.896 RL 82.413 IP CH -24.896 RL 82.263 =VTP CH -19.896 RL 82.283= 593.957 RL 85.081 1 570.426 RL 84.427 IP CH 608.957 CH 555.426 VTP CH VERT. CURVE LENGTH (m) 10.000m R 294.2m 30.000m R 582.6m VERT. CURVE RADIUS (m) VERT. GEOMETRY GRADE (%) -2.999% 11.172m 0.400% -0.200% VERT. GEOMETRY LENGTH(m) 484.745m 95.577m **DATUM RL 62.000** HORZ. CURVE LENGTH (m) 19.952m 39.397m 39.397m R -50.000m HORZ. CURVE RADIUS (m) R 20.000m R 20.000m EXISTING SURFACE LEVELS 80.564 80.697 82.612 82.599 80.784 82.600 82.604 82.643 82.754 82.788 82.903 82.860 82.277 82.754 82.724 ROAD CENTRELINE CUT / FILL DEPTH 1.602 2.391 TO EXISTING SURFACE DESIGN LEVELS 82.280 82.282 84.041 84.038 84.111 84.192 84.762 84.540 84.693 84.202 85.294 ROAD CENTRELINE 82. 83 83 CONTROL LINE CHAINAGE 459.849 460.000 540.000 542.441 613.869 640.000 643.932 380.000 -21.073 -20.000 ROAD CENTRELINE MC02 - ROAD 2 SCALE: H 1:1000 V 1:100 KALFRESH PTY LTD

SCALE 1:1000

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MC02 LONGITUDINAL SECTION - SHEET 01 AHD Level 6, Springfield Tower, 145 Sinnathamby Boulevard

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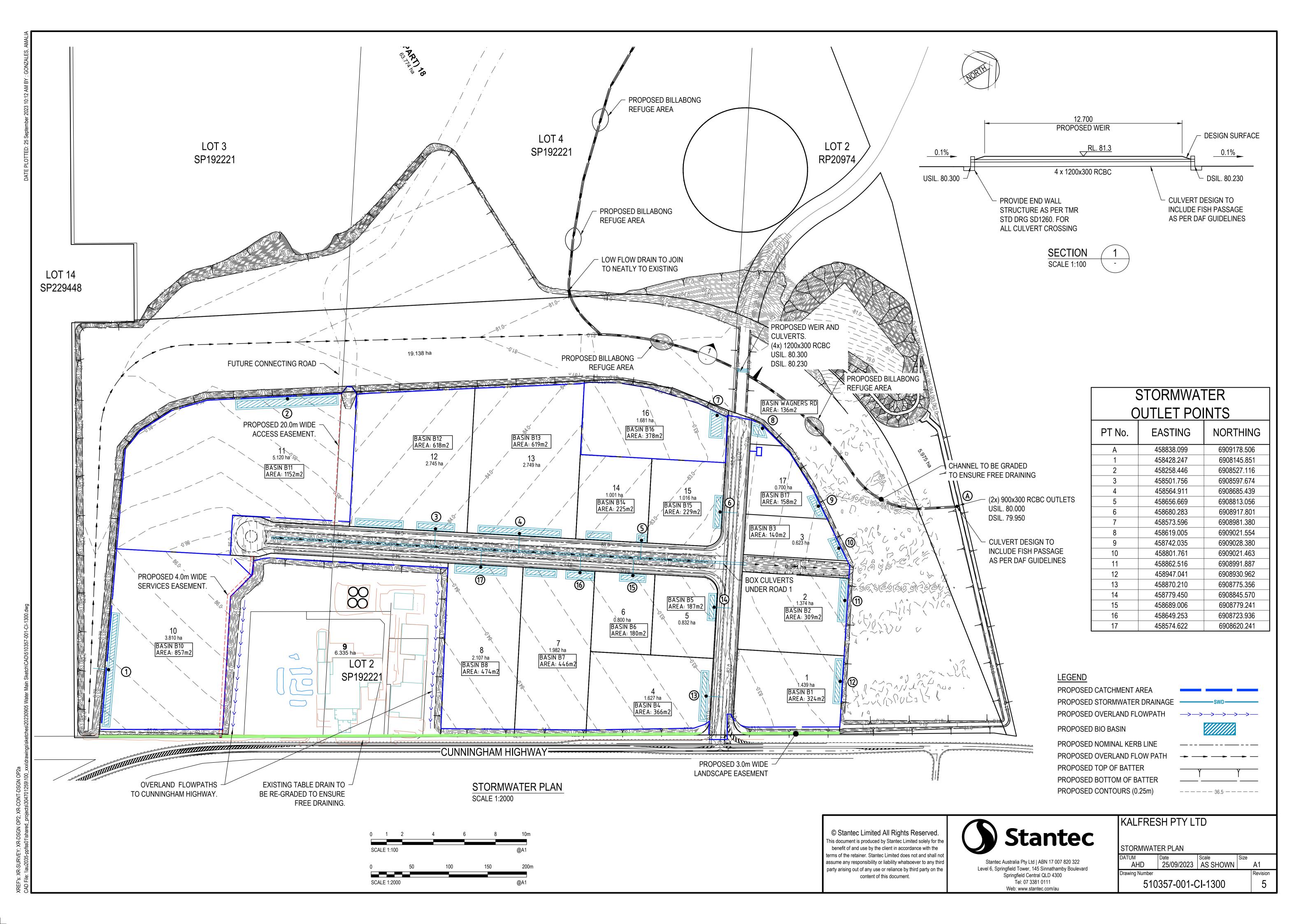
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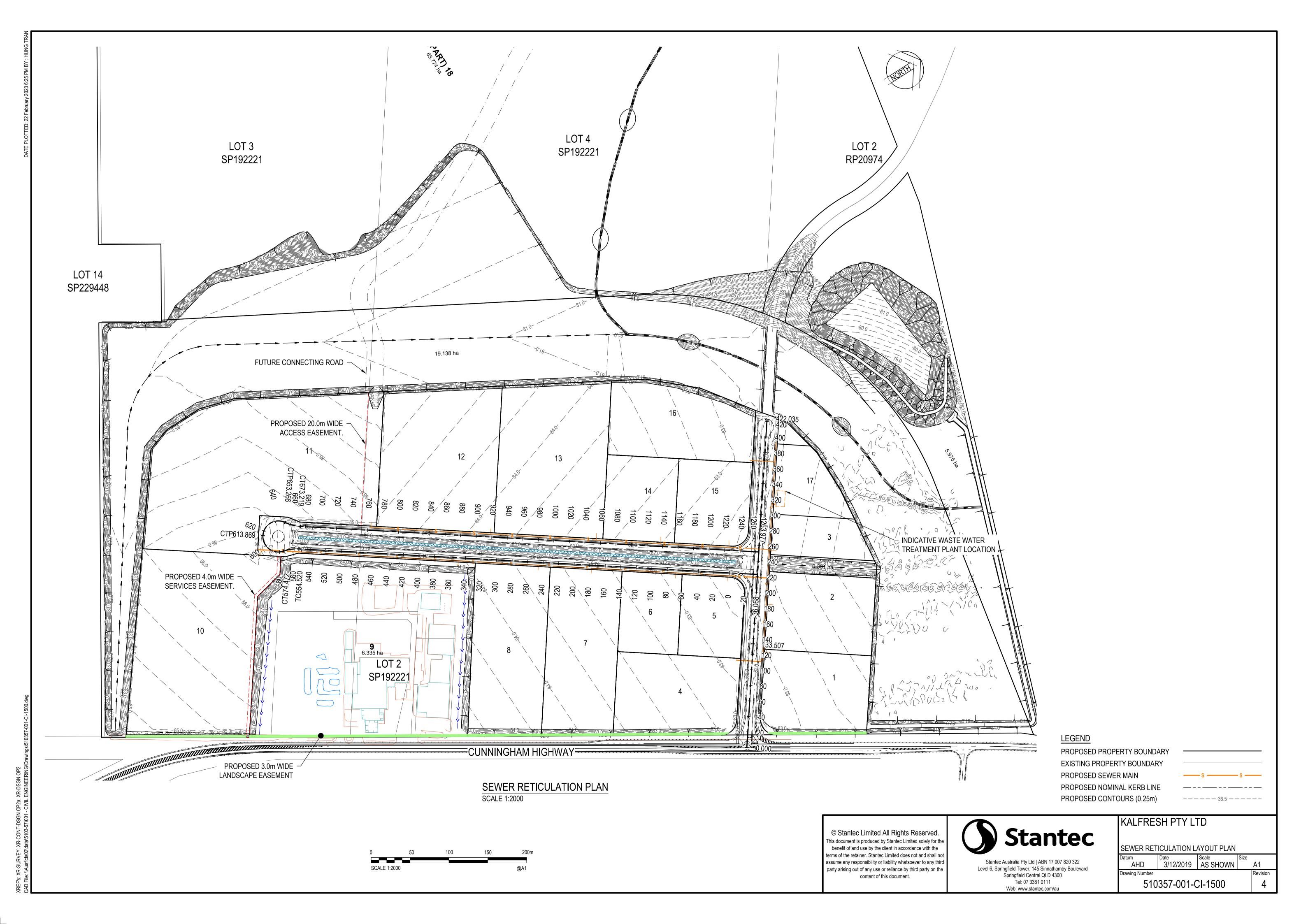
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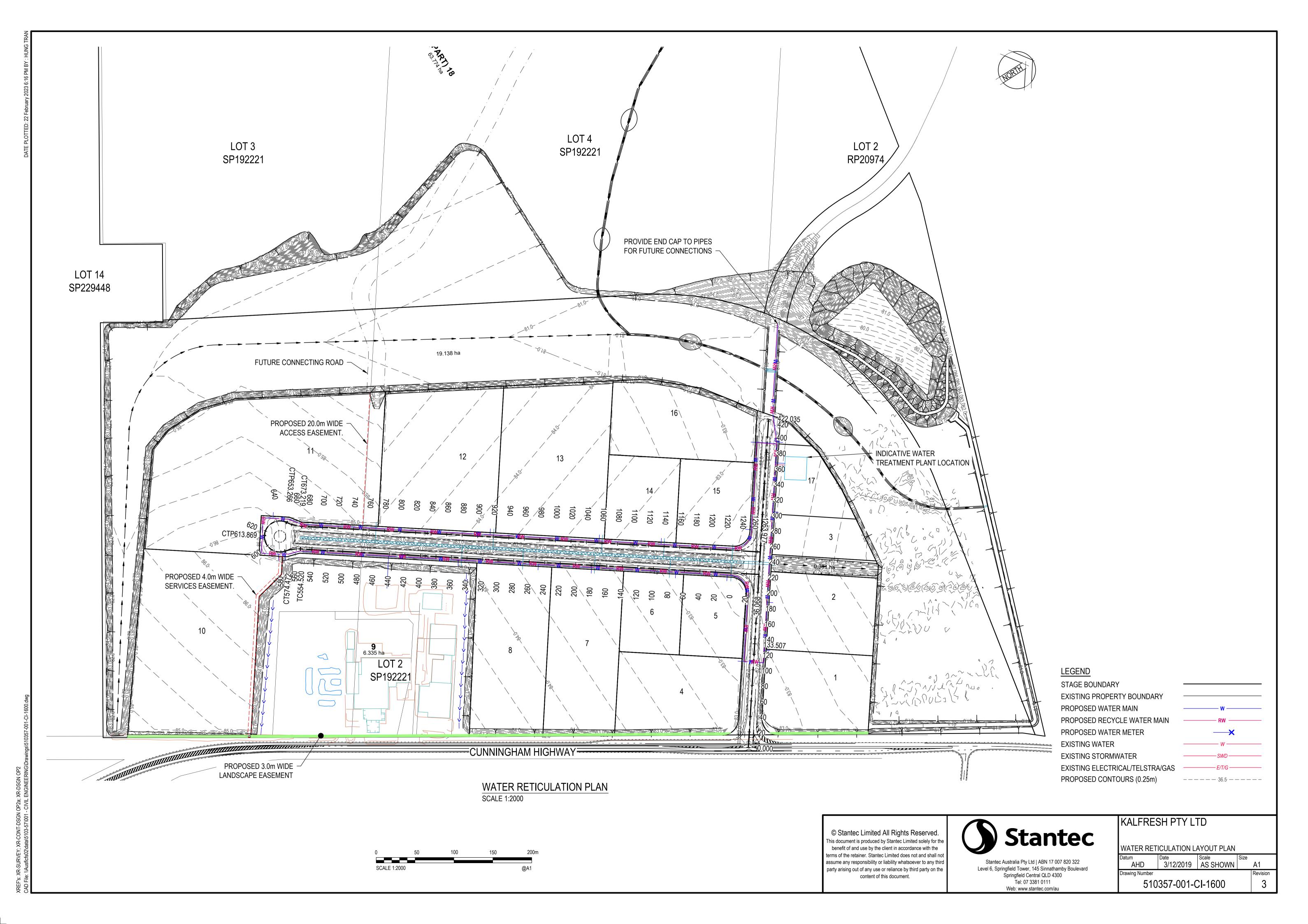
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RT. CURVE LENGTH (m)		VTP CH 656.735 RL 84.365	30.000m R 1167.11	✓ VTP CH 686.735 RL 84.040					IP CH 767.889 RL 84.202																								VTP CH 1252.473 RL 82.264		
RT. CURVE RADIUS (m) RT. GEOMETRY GRADE (%) RT. GEOMETRY LENGTH(m) TUM RL 62.000		-2.3719 62.778	/ <sub>6</sub>			0.200% 96.154m			><												-0.400%  -0.400%  -0.400%												3.		
ORZ. CURVE LENGTH (m) ORZ. CURVE RADIUS (m)	39. R 20	0.397m 19.	953m 0.000m																																
STING SURFACE LEVELS AD CENTRELINE	82.724	82.677 82.664	82.585	82.523	82.478	82.375	82.249	82.732	82.505	82.175	82.155	82.046	81.986	81.915	81.833	81.790	81.694	81.560	81.570	81.464	81.241	81.360	81.008	81.153	81.095	81.087	81.002	80.948	80.921	80.851	80.815	80.726	80.751		
7 / FILL DEPTH EXISTING SURFACE	1.945	1.771	1.506	1.514	1.588	1.732	1.898	1.454	1.697	1.898	1.838	1.868	1.847	1.839	1.841	1.803	1.819	1.873	1.784	1.809	1.952	1.753	2.026	1.800	1.779	1.707	1.711	1.686	1.632	1.622	1.579	1.588	1.510		
IGN LEVELS AD CENTRELINE	84.669	84.448 84.292	84.091	84.037	84.066	84.106	84.146	84.186	84.202	•   •	83.994	83.914	83.834	83.754	83.674	83.594	83.514	83.434	83.354	83.274	83.194	83.114	83.034	82.954	82.874	82.794	82.714	82.634	82.554	82.474	82.394	82.314	82.261		
NTROL LINE CHAINAGE AD CENTRELINE	543.932	653.266 660.000	673.219		000.00	720.000	740.000	160.000	767.889	000.008	820.000	340.000	360.000	380.000	900.000	320.000	940.000	960.000	000.086	000.000	020.000	040.000	1060.000	1080.000	100.000	120.000	140.000	160.000	180.000	200.000	220.000	1240.000	1253.650 1260.000		





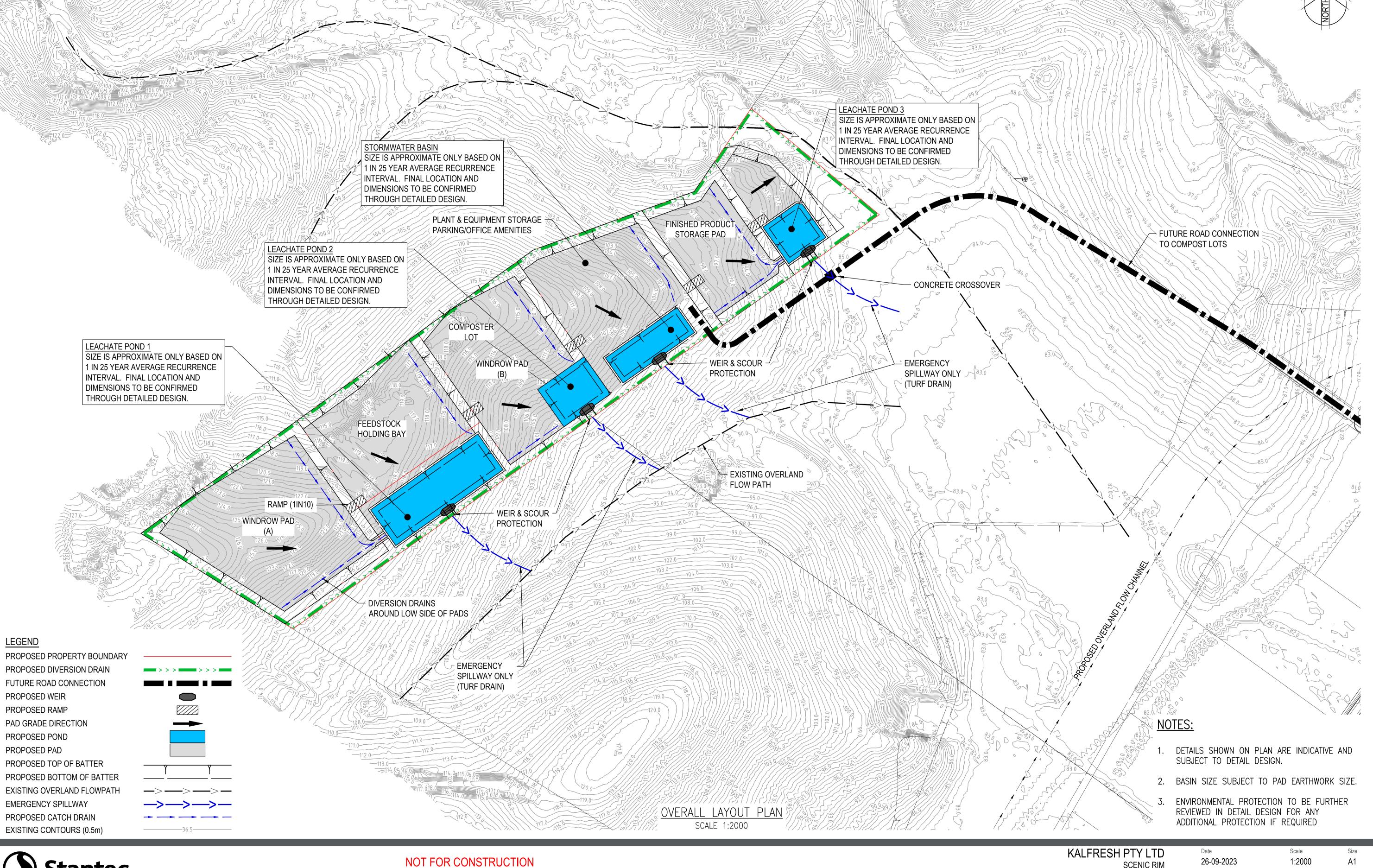


**APPENDIX** 

C

COMPOST PAD STORMWATER LAYOUT







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APPENDIX

WATER AND WASTEWATER RETICULATION SCHEMATICS



